#### IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Application No.:

U.S. National Serial No.:

Filed:

PCT International Application No.:

PCT/FR2003/002317

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Date: January 18, 2005

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PCT/FR2003/002317

WO 2004/013403

METHOD FOR THE TREATMENT OF ARCHITECTURAL TEXTILES BY
MEANS OF IMPREGNATION WITH A SILICONE COMPOSITION THAT

CAN BE CROSSLINKED INTO AN ELASTOMER, AND ARCHITECTURAL

TEXTILE COATED BY MEANS OF SAID METHOD

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The invention relates to the treatment of fibrous materials (in particular flexible supports such as woven supports or nonwoven supports) with a silicone elastomer composition that can be vulcanized by hydrosilyation (or polyaddition), especially of the two-component (RTV-2) type.

More specifically, the invention relates to the preparation of architectural silicone membranes obtained by impregnation of an architectural textile, in particular but non-limitingly of a glass fabric or of a fabric made of synthetic fibers, such as a polyester, using the silicone composition, especially of RTV2 type, targeted above.

The invention also relates to architectural silicone membranes obtained by impregnation of an architectural textile, in particular but non-limitingly of a glass fabric, using the silicone composition, especially of RTV2 type, targeted above.

The term "architectural textile" is understood to mean a woven or nonwoven fabric, and more generally any fibrous support intended, after coating, for making up:

- shelters, movable structures, textile buildings, partitions, flexible doors, tarpaulins, tents, stands or marquees;
- furniture, claddings, billboards, windshields or filter panels;
  - solar protection panels, ceilings and blinds.

The treatment of architectural textiles by means of liquid silicone compositions that can be crosslinked into elastomers, is conventionally carried out by coating or by impregnation when the compositions are emulsions or solutions.

Silicone coating is defined as the action of

using a а textile, crosslinkable silicone composition, and then of crosslinking the film coated on the support, so as to produce a coating intended in particular to protect it and to give it for particular properties, example to give hydrophobic/oleophobic and impermeable characteristics or improved mechanical properties or else suitable for modifying the appearance thereof.

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Impregnation is defined as the action of making 10 a highly fluid crosslinkable silicone-based liquid penetrate into a fibrous support (penetration right to the core) and then in causing the silicone to crosslink in order to give the textile properties of the type mentioned above.

In practice, silicone elastomer coatings on architectural textiles have many advantages owing to the intrinsic characteristics of silicones. These composites have in particular good flexibility, good mechanical strength and improved fire behavior.

Moreover, unlike conventional elastomers, silicones give them *inter alia* suitable protection owing to their hydrophobicity and to their excellent chemical, thermal and environmental resistance, and also long lifetime.

25 However, in the emerging field of silicone composites for textile architecture, the method of depositing the silicones by coating may be deficient. This is because architectural fabrics exposed to the weather must not be subject to the effect of capillary 30 rise from the edges, which would impair aesthetics and their lifetime. Moreover, coating does not represent an effective technique for protecting fibrous materials from the phenomenon of capillary rise.

To alleviate this, it is conceivable a priori to use the technique of impregnating textiles by means of liquid silicone compositions, for example of the RTV-2 type, which can be crosslinked into elastomers.

However, the only liquid silicone compositions

known hitherto for impregnating textiles are fluid silicone solutions or emulsions.

In fact, before the invention there was a technical preconception that liquid silicone compositions consisting of silicone oils, for example of the RTV-2 type, could not be used for impregnating textiles.

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Notwithstanding this, the inventors have sought to develop a method for the treatment at least by 10 impregnation of architectural textiles, by applying a liquid silicone composition based on one or more oils, which can be crosslinked into an elastomer, it being necessary for the said method to have in particular specifications making it possible to 15 architectural textiles treated right to the core and on the surface, so as to exhibit improved properties in terms of mechanical reinforcement, water repellency, impermeability, appearance, fireproofing and above all resistance to capillary rise.

Another objective of the inventors is the manufacture of architectural silicone membranes formed by composites based on architectural textiles and on silicone, which membranes have good mechanical properties and resistance to capillary rise, which composites can be produced by impregnation according to the method of the invention.

These objectives, among others, were achieved who by the inventors have discovered, surprisingly, and despite the aforementioned technical preconception, that a liquid silicone composition whose liquid phase is essentially, if not exclusively, formed by one or more silicone oils that can be crosslinked, especially at room temperature, into an elastomer can be used in a method for the treatment by impregnation of fibrous supports in order to give them mechanical properties and capillary rise resistance properties that are very satisfactory.

It therefore follows that the invention first of all relates to a method for the preparation of an

architectural silicone membrane by impregnation of an architectural textile with at least one silicone, comprising the following essential stages:

-Ii = positive integer-

- application to an architectural textile of a liquid silicone composition which can be crosslinked into an elastomer, comprising:
  - (a) at least one polyorganosiloxane (POS) having, per molecule, at least two alkenyl, preferably  $C_2-C_6$ , groups linked to the silicon;
  - (b) at least one polyorganosiloxane having, per molecule, at least three hydrogen atoms linked to the silicon;
- (c) a catalytically effective quantity of at 15 least one catalyst, preferably composed of at least one metal belonging to the platinum group;
  - (d) optionally, at least one adhesion promoter;
  - (e) optionally, a mineral filler;
- (f) optionally, at least one crosslinking
  20 inhibitor;
  - (g) optionally, at least one polyorganosiloxane resin; and
  - (h) optionally, functional additives in order to impart specific properties;
- - III -

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optionally at least one other operating sequence comprising stages Ii  $\geq$  2 and Iii  $\geq$  2 (i being a positive integer) corresponding to the same definition as that given above for stages Ii and IIi;

characterized in that stage Ii=1 is a stage of impregnation right to the core of the architectural textile using a liquid silicone composition which is as defined above and which is furthermore fluid and obtained without having recourse either to dilution or to dissolution or to emulsification.

To the knowledge of the inventors, such fluid

compositions based on reactive silicone oils capable of curing by polyaddition have never been used in a method for impregnating fibrous materials.

Such fluid liquid silicone compositions (oils) preferably have a dynamic viscosity of between 1000 and 7000 mPa.s, at 25°C, and more preferably of between 2000 and 5000 mPa.s at 25°C before crosslinking.

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All the viscosities mentioned in the present application correspond to a dynamic viscosity quantity at 25°C, that is to say the dynamic viscosity thus measured, in a manner known per se, at a shear rate gradient low enough for the measured viscosity to be independent of the rate gradient.

Advantageously, the oily fluid liquid silicone composition selected for the impregnation stage (Ii = 1) has, after complete crosslinking by thermal action, that is, curing in a fan oven for 30 minutes at 150°C, at least one of the following mechanical properties:

- a Shore A hardness of at least 2, preferably between 5 and 65;
  - a tensile strength of at least 0.5 N.mm<sup>-1</sup>, preferably of at least 1.0 N.mm<sup>-1</sup> and more preferably of at least 2.0 N.mm<sup>-1</sup>;
- an elongation at break of at least 50%, preferably at least 100% and more preferably of at least 200%.

The general techniques for impregnating architectural textiles are well known to those skilled in the art: knife, in particular by knife-over-rule, floating knife and knife-over-belt, or by padding, that is to say by squeezing between two rolls, or also by lick roll, rotary machine, reverse roll, transfer or spraying.

One or both faces of a textile material can be 35 impregnated, preferably by padding. Drying crosslinking, preferably by hot air or infrared radiation, especially from 30 s to 5 min, at a crosslinking temperature not exceeding the decomposition temperature of the support, are

subsequently carried out.

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Padding represents one technique particularly suitable for the method of the invention.

According to a preferred embodiment of the method according to the invention, provision is made for at least one stage III, in which stage Ii  $\geq$  2 for application of liquid silicone is a coating using a liquid silicone composition that can be crosslinked into an elastomer.

The fact of carrying out a treatment that combines at least one impregnation with at least one coating with a silicone is a guarantee of quality as regards the architectural textiles whose properties it is desired to modify, especially its resistance to capillary rise, without impairing the other mechanical, water repellency, fire resistance and appearance properties.

The fluidity of the crosslinkable liquid silicone coating composition of stage Ii  $\geq$  2 is identical to or different from that of the impregnation stage Ii = 1.

Advantageously, the fluidity of the silicone coating liquid is lower than that of the silicone impregnation liquid.

The silicone oil compositions, including the fluid impregnation compositions, employed in the method according to the invention comprise a blend of polyorganosiloxanes (a) and (b).

The polyorganosiloxanes (a) used in the present invention preferably have units of formula:

$$W_a Z_b SiO_{(4-(a+b))/2}$$
 (a.1)

in which:

- W is an alkenyl group;
- Z is a monovalent hydrocarbon group, which has no unfavorable effect on the activity of the catalyst and chosen from alkyl groups having from 1 to 8 carbon atoms inclusive, optionally substituted with at least one halogen atom, and from aryl groups;
  - a is 1 or 2, b is 0, 1 or 2 and a + b is

between 1 and 3; and

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- optionally, at least one portion of the other units are units of average formula:

$$Z_cSiO_{(4-c)/2}$$
 (a.2)

5 in which W has the same meaning as above and c has a value between 0 and 3.

The polyorganosiloxane (a) may be predominantly formed from units of formula (a.1) or it may also contain units of formula (a.2). Likewise, it may have a linear structure and its degree of polymerization is preferably between 2 and 5000.

 $\,$  W is generally chosen from methyl, ethyl and phenyl radicals, at least 60 mol% of the radicals W being methyl radicals.

Examples of siloxyl units of formula (a.1) are the vinyldimethylsiloxane unit, the vinylphenylmethylsiloxane unit and the vinylsiloxane unit.

Examples of siloxyl units of formula (a.2) are the  $SiO_{4/2}$ , dimethylsiloxane, methylphenylsiloxane, diphenylsiloxane, methylsiloxane and phenylsiloxane units.

Examples of polyorganosiloxanes (a) are dimethylvinylsilyl-terminated dimethylpolysiloxanes, trimethylsilyl-terminated methylvinyldimethylpolysiloxanes copolymers, dimethylvinylsilyl-terminated methylvinyldimethylpolysiloxane copolymers and cyclic methylvinylpolysiloxanes.

The dynamic viscosity  $\eta_d$  of this polyorganosiloxane (a) is between 0.01 and 200 Pa.s, preferably between 0.1 and 100 Pa.s.

Preferably, the POS (a) comprises at least 98% of siloxyl units D:  $-R_2SiO_{2/2}$  where R satisfies the same definition as W or Z, this percentage corresponding to a number of units per 100 silicon atoms.

As regards the silicone oil compositions according to the invention, the preferred polyorganosiloxane (b) compositions contain siloxyl units of formula:

in which:

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- L is a monovalent hydrocarbon group, which has no unfavorable effect on the activity of the catalyst and chosen from alkyl groups having from 1 to 8 carbon atoms inclusive, optionally substituted with at least one halogen atom, and from aryl groups;
- d is 1 or 2, e is 0, 1 or 2 and d + e has a value between 1 and 3;
- optionally, at least one portion of the other 10 units being units of average formula:

 $L_g SiO_{(4-q)/2}$  (b.2)

in which L has the same meaning as above and g has a value between 0 and 3.

As examples of polyorganosiloxanes (b), mention 15 may be made of poly(dimethylsiloxane) (methylhydrogenosiloxy)- $\alpha$ , $\omega$ -dimethylhydrogenosiloxane.

The polyorganosiloxane (b) may be formed only from units of formula (b.1) or may also include units of formula (b.2).

The polyorganosiloxane (b) may have a linear, branched, cyclic or network structure. The degree of polymerization is greater than or equal to 2 and more generally is less than 100.

The dynamic viscosity  $\eta_d$  of this polyorgano- 25 siloxane (b) is between 5 and 1000 mPa.s, preferably between 10 and 100 mPa.s.

The group L has the same meaning as the group  $\ensuremath{\mathtt{Z}}$  above.

Examples of units of formula (b.1) are:  $30 \text{ H}(CH_3)_2SiO_{1/2}$ ,  $HCH_3SiO_{2/2}$  and  $H(C_6H_5)SiO_{2/2}$ .

The examples of units of formula (b.2) are the same as those given above in the case of the units of formula (a.2).

Examples of polyorganosiloxanes (b) are:

- hydrogenodimethylsilyl-terminated dimethylpolysiloxanes;
  - copolymers containing trimethylsilylterminated (dimethyl)-(hydrogenomethyl)polysiloxane units;

- copolymers containing hydrogenodimethylsilylterminated dimethyl-hydrogenomethylpolysiloxane units;
- trimethylsilyl-terminated hydrogenomethylpolysiloxanes;

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- cyclic hydrogenomethylpolysiloxanes; and
- hydrogenosiloxane resins containing siloxyl units M:  $R_3SiO_{1/2}$ , Q:  $SiO_{4/2}$  and/or T:  $RSiO_{3/2}$  and optionally D:  $R_2SiO_{2/2}$ , with R = H or satisfying the same definition as L.
- 10 As other examples of monovalent hydrocarbon groups Z or L that can be present in the abovementioned POSs (a) and (b), mention may be made of: methyl; ethyl; n-propyl; isopropyl; n-butyl; isobutyl; tertbutyl; chloromethyl; dichloromethyl;  $\alpha$ -chloroethyl; 15  $\alpha,\beta$ -dichloroethyl; fluoromethyl; difluoromethyl;  $\alpha, \beta$ -difluoroethyl, 3,3,3-trifluoropropyl; trifluoro-4,4,4-trifluorobutyl; 3,3,5,5,5,5-hexacyclopropyl; fluoropentyl;  $\beta$ -cyanoethyl;  $\gamma$ -cyanopropyl; phenyl; p-chlorophenyl; m-chlorophenyl; 3,5-dichlorophenyl; 20 trichlorophenyl; tetrachlorophenyl; o-, p- or m-tolyl;  $\alpha, \alpha, \alpha$ -trifluorotolyl; 2,3-dimethylphenyl; xylyl; 3,4-dimethylphenyl.

These groups may optionally be halogenated, or else may be chosen from cyanoalkyl radicals.

25 The halogens are for example fluorine, chlorine, bromine and iodine, preferably chlorine or fluorine.

The POSs (a) and (b) may consist of blends of various silicone oils.

Preferably, the proportions of (a) and of (b) are such that the molar ratio of the hydrogen atoms linked to the silicon in (b) to the alkenyl radicals linked to the silicon in (a) is between 0.4 and 10.

According to a variant, the silicone phase of the composition comprises at least one polyorganosiloxane resin (g) containing at least one alkenyl residue in its structure, and this resin has a weight content of alkenyl groups of between 0.1 and 20% by weight and preferably between 0.2 and 10% by weight. These resins are well-known branched organopolysiloxane

oligomers or polymers that are commercially available. Preferably, they are in the form of siloxane solutions and have, in their structure, at least two different units chosen from those of formula  $R_3SiO_{0.5}$  (M unit),  $R_2SiO$  (D unit),  $RSiO_{1.5}$  (T unit) and  $SiO_2$  (Q unit), at least one of these units being a T or Q unit.

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The radicals R are identical or different and are chosen from  $C_1$ - $C_6$  linear or branched alkyl radicals,  $C_2$ - $C_4$  alkenyl radicals, phenyl and 3,3,3-trifluoropropyl. As alkyl radicals R, mention may be made, for example, of methyl, ethyl, isopropyl, tert-butyl and n-hexyl radicals and, as alkenyl radicals R, vinyl radicals.

It should be understood that some of the radicals R in the resins (g) of the aforementioned type are alkenyl radicals.

examples of branched organopolysiloxane oligomers or polymers, mention may be made of MQ resins, MDQ resins, TD resins and MDT resins, it being possible for the alkenyl functional groups carried by the M, D and/or T units. As examples of resins that are particularly suitable, mention may be made of vinyl-containing MDQ or MQ resins having a weight content of vinyl groups of between 0.2 and 10% by weight, these vinyl groups being carried by the M and/or units. This structure D of resin advantageously present in a concentration of between 10 and 70% by weight, preferably between 30 and 60% by weight and even more preferably between 40 and 60% by weight relative to all of the constituents of the composition.

The polyaddition reaction is well those skilled in art. It is also possible to use a catalyst in this reaction. Such а catalyst especially be chosen from platinum and rhodium compounds. In particular, it is possible complexes of platinum and an organic substance, described in patents US-A-3 159 601, US-A-3 159 602 and US-A-3 220 972 and European patents EP-A-0 057 459, EP-

A-0 188 978 and EP-A-0 190 530, complexes of platinum with a vinyl-containing organosiloxane, which are described in patents US-A-3 419 593, US-A-3 715 334, US-A-3 377 432 and US-A-3 814 730. The catalyst generally preferred is platinum. In this case, the quantity by weight of catalyst (c), calculated by weight of platinum metal, is generally between 2 and 400 ppm and preferably between 5 and 100 ppm, these values being based on the total weight of the polyorganosiloxanes (a) and (b).

In one advantageous method of implementing the process according to the invention, an adhesion promoter may be used. This adhesion promoter may for example comprise:

15 (d.1) at least one alkoxylated organosilane satisfying the following general formula:

$$R^{3}R^{2}C = C \times (A)_{x} \times Si \times (OR^{5})_{3-x}$$

$$(d.1)$$

in which:

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- $R^1$ ,  $R^2$ ,  $R^3$  are hydrogenated or hydrocarbon 20 radicals, which are the same or differ from one another and represent hydrogen, a  $C_1$ - $C_4$  linear branched alkyl or a phenyl optionally substituted with at least one  $C_1$ - $C_3$  alkyl;
  - A is a  $C_1$ - $C_4$  linear or branched alkylene;
- 25 G is a valency bond;
  - $R^4$  and  $R^5$  are radicals, which are identical or different and represent a linear or branched  $C_1\text{-}C_4$  alkyl;
    - x' = 0 or 1; and
- 30 x = 0 to 2,

said compound (d.1) being preferably vinyltrimethoxysilane (VTMS);

(d.2) at least one organosilicone compound comprising at least one epoxy radical, said compound (d.2) being 35 preferably 3-glycidoxypropyltrimethoxysilane (GLYMO); and (d.3) at least one metal M chelate and/or a metal alkoxide of general formula  $M(OJ)_n$ , where n= valency of M and  $J=C_1-C_8$  linear or branched alkyl, M being chosen from the group formed by: Ti, Zr, Ge, Li, Mn, Fe, Al and Mg, said compound (d.3) preferably being tert-butyl titanate.

The proportions of (d.1), (d.2) and (d.3), expressed as a percent by weight relative to the total of the three, are preferably the following:

 $(d.1) \ge 10$ ,

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 $(d.2) \ge 10$ ,

 $(d.3) \leq 80.$ 

Moreover, this adhesion promoter (d) is preferably present in an amount of 0.1 to 10%, preferably 0.5 to 5% and even more preferably 1 to 2.5% by weight relative to all of the constituents of the composition.

It is also possible to provide a filler (e), which will preferably be a mineral filler. It may consist of the products chosen from siliceous (or nonsiliceous) materials.

With regard to siliceous materials, these may act as a reinforcing or semireinforcing filler.

The reinforcing siliceous fillers are chosen 25 from colloidal silicas, fumed silica powders, precipitated silica powders or mixtures thereof.

These powders generally have a mean particle size of less than 0.1  $\mu m$  and a BET specific surface of greater than 50  $m^2/g$ , preferably between 100 and 300  $m^2/g$ .

The semireinforcing siliceous fillers, such as diatomaceous earths or ground quartz, may also be employed.

As regards the nonsiliceous mineral materials, these may act as semireinforcing mineral filler or bulking filler. Examples of these nonsiliceous fillers that can be used by themselves or as a mixture are carbon black, titanium dioxide, aluminum oxide, hydrated alumina, expanded vermiculite, zirconia, a

zirconate, unexpanded vermiculite, calcium carbonate, zinc oxide, mica, talc, iron oxide, barium sulfate and slaked lime. These fillers have a particle size generally between 0.01 and 300  $\mu m$  and a BET surface area of less than 100 m<sup>2</sup>/g.

For practical purposes the filler employed is a silica, but this is in no way limiting.

The filler may be treated by means of any suitable compatibilizing agent, especially hexamethyldisilazane. For further details in this regard, the reader may refer for example to patent FR-B-2 764 894.

As regards weights, it is preferred to use a quantity of filler of between 5 and 30%, preferably between 7 and 20%, by weight relative to all of the constituents of the composition.

Advantageously, the silicone elastomer composition furthermore includes at least one retarder (f) (or crosslinking inhibitor) for retarding the addition reaction, chosen from the following compounds:

- polyorganosiloxanes, advantageously cyclic polyorganosiloxanes substituted with at least one alkenyl, tetramethylvinyltetrasiloxane being particularly preferred;
  - pyridine;
- 25 organic phosphines and phosphites;
  - unsaturated amides;
  - alkyl maleates; and
  - acetylenic alcohols.

These acetylenic alcohols (cf. FR-B-1 528 464 30 and FR-A-2 372 874), which are included among the preferred hydrosilylation reaction thermal blockers, have the formula:

in which formula:

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- R is a linear or branched alkyl radical or a
  phenyl radical;
  - R' is H or a linear or branched alkyl radical or a phenyl radical;
    - it being possible for the R, R' radicals and

the carbon atom situated  $\alpha$  to the triple bond to optionally form a ring;

- the total number of carbon atoms contained in R and R' being at least 5, preferably from 9 to 20.

Said alcohols are preferably chosen from those having a boiling point above 250°C. As examples, mention may be made of:

- 1-ethynyl-1-cyclohexanol;
- 3-methyl-1-dodecyn-3-ol;
- 10 3,7,11-trimethyl-1-dodecyn-3-ol;

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- 1,1-diphenyl-2-propyn-1-ol;
- 3-ethyl-6-ethyl-1-nonyn-3-ol; and
- 3-methyl-1-pentadecyn-3-ol.

These  $\alpha\text{-cetylenic}$  alcohols are commercially available products.

Such a retarder (f) is present in an amount of 3000 ppm at most, preferably in an amount of 100 to 2000 ppm relative to the total weight of the organopolysiloxanes (a) and (b).

With regard to the functional additives (h) that can be employed, these may be covering products, such as for example pigments/dyes or stabilizers.

In the method according to the invention it is also possible to use a two-component precursor system for the composition. This two-component system is characterized in that:

- it is in two separate parts A and B that are intended to be mixed together to form the composition, and in that one of these parts A and B contains the catalyst (c) and only one polyorganosiloxane species (a) or (b); and
- part A or B containing the polyorganosiloxane (b) contains no compound (d.3) of the promoter (d).

The composition may therefore for example, 35 consist of a part (a) comprising the compounds (d.1) and (d.2), while part (b) contains the compound (d.3), in order to obtain the two-component silicone elastomer composition A-B.

If a filler is used, it is advantageous firstly

to prepare a primary paste by mixing a mineral filler with at least some of the POS (b) and at least some of the polyorganosiloxane (a).

This paste serves as a basis for obtaining, on the one hand, a part A resulting from mixing the latter with the polyorganosiloxane (b), optionally a crosslinking inhibitor and finally the compounds (d.1) and (d.2) of the promoter (d). The part B is produced by mixing some of the abovementioned paste with polyorganosiloxane (a), with catalyst (Pt) and with compounds (d.3) of the promoter (d).

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The viscosity of the parts A and B and of their mixture can be adjusted by varying the quantities of the constituents and by choosing polyorganosiloxanes of different viscosity.

If one or more functional additives (h) are employed, they are distributed in the parts A and B according to their affinity with the content of A and B.

Once the parts A and B have been mixed together, they form a ready-to-use silicone elastomer composition (RTV-2) which can be applied on the support by any suitable impregnation means (for example, padding) and optionally any suitable impregnation means (for example a knife or roll).

The crosslinking of the liquid (fluid) silicone composition applied on the architectural textile to be impregnated, or even coated, is generally activated for example by heating the impregnated, or coated, architectural textile to a temperature of between 50 and 200°C, while obviously taking into account the maximum heat resistance of the support.

Another subject of the invention is composed of an architectural silicone membrane that can be obtained by the method according to the invention (architectural textile/silicone composite).

This composite membrane is characterized in that it is impregnated right to the core with crosslinked silicone elastomer obtained from a liquid

silicone composition as defined above in the context of the description of the method according to the invention, this composition furthermore being fluid and obtained without having recourse either to dilution or to dissolution or to emulsification.

Advantageously, the architectural textile which is a constituent of this membrane is formed by a woven fabric, a nonwoven fabric, a knit or more generally any fibrous support chosen from the group of materials comprising: glass, silica, metals, ceramic, silicon carbide, carbon, boron, basalt, natural fibers, such as cotton, wool, hemp, flax; artificial fibers, such as viscose or cellulose fibers; synthetic fibers, such as polyesters, polyamides, polyacrylics, "chlorofibres", polyolefins, synthetic rubbers, polyvinyl alcohol, aramides, "fluorofibres", phenolics, etc.

The subject of the invention is also an architectural silicone membrane (architectural textile crosslinked silicone elastomer composite) that can be obtained by the method according to the invention or from the abovementioned two-component system, characterized by a capillary rise of less than 20 mm, preferably of less than 10 mm and more preferably still equal to 0, the capillary rise being measured according to a T test.

Advantageously, the architectural silicone membrane corresponding to a coated architectural textile as defined above obtained by the process described above constitutes a membrane of choice for interior or exterior architecture or solar protection, especially because of its low, indeed even zero capillary rise.

According to a preferred characteristic, such a 35 membrane has a weight of less than  $2000 \text{ g/m}^2$  and preferably a weight of between  $400 \text{ and } 1500 \text{ g/m}^2$ .

#### Description of the figures:

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Figure 1 is a micrograph of a section through a

silicone composite based on fibrous material.

Figure 2 is a diagram showing the results of a T test for comparing capillary rise, carried out on three strips of fabric,  $\alpha$  (control) and  $\beta a$ ,  $\beta b$  (Example I.7).

The following examples have been given for the purpose of illustrating particular embodiments of architectural silicone membranes according to the invention, without limiting the latter to these simple particular embodiments.

## EXAMPLE I: Preparation, impregnation and properties of a silicone oil composition according to the invention

#### 15 <u>I.1 - Preparation</u>

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The following materials were progressively mixed, in a reactor at room temperature, in the proportions indicated below (in parts by weight):

- 96.6 parts of an MM(Vi)D(Vi)DQ resin containing
  20 about 0.6% Vi;
  - 11 parts of poly(diMe)(Mehydrogenosiloxy)-  $\alpha$ ,  $\omega$ -diMehydrogenosiloxy, having a viscosity of 25 mPa.s and containing 20% SiH;
    - 0.025 parts of a ethynylcyclohexanol;
- 25 1 part of vinyltrimethoxysilane;
  - 1 parts of 3-glycidoxypropyltrimethoxysilane;
  - 0.4 parts of butyl titanate;
  - 0.022 parts of Karstedt's platinum crosslinking catalyst.
- 30 NB: Me corresponds to a methyl radical.

### I.2 - Properties of the composition thus prepared - Viscosity:

The viscosity of the composition prepared was measured by means of a Brookfield viscometer: viscosity = 2.3 Pa.s.

#### Reactivity:

The reactivity of the bath was assessed by measuring its gel time in a Gel Timer GelNorm sold by

OSI: reactivity at  $70^{\circ}C = 30$  minutes.

#### I.3 - Impregnation

I.3.a A  $200 \text{ g/m}^2$  woven polyester fabric was impregnated with the composition by means of a laboratory calender. The impregnation conditions were the following:

- diameter of the rolls: 10 cm (width 25 cm)

- run speed:

1 m/min

- applied pressure:

20 kg/cm

- degree of squeezing:

35%

I.3.b A 300  $g/m^2$  woven glass fabric was impregnated with the composition by means of a laboratory calender.

15 The impregnation conditions were the following:

- diameter of the rolls: 10 cm (width 25 cm)

- run speed:

1 m/min

- applied pressure:

22 kg/cm

- degree of squeezing:

30%

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#### I.4 - Crosslinking

The silicone composition deposited was crosslinked by placing the architectural membrane (composite) resulting from test I.3-a or I.3-b in a fan oven at  $150^{\circ}$ C for 1 minute.

# <u>I.5 - Mechanical properties of the silicone</u> impregnation elastomer after crosslinking

The mechanical usage properties were measured according to the standards of the art on the basis of a pin 6 mm in thickness as regards hardness and a test plaque 2 mm in thickness for the tensile strength experiments. The crosslinking was completed by curing in a fan oven at 150°C for 30 minutes.

35 Shore A hardness:

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Tensile strength:

3.9 MPa

Elongation at break:

140%.

### I.6 - Inspection of the impregnation

The penetration of the composition into the fabric was observed using scanning electron microscopy.

The micrograph in Figure 1 shows a sectional view of the composite obtained from Example I.3-a. The corresponding scale is displayed on the image. It demonstrates the quality of the impregnation, revealing the compactness of the resulting composite. This micrograph shows the quality of the impregnation obtained by the process forming the subject of the invention. The absence of fluidizing solvent or emulsion prevents the formation of solvent pockets in the matrix of the crosslinked silicone composition.

#### I.7 - Resistance to capillary rise

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#### Analytical procedure:

The capillary rise is given by the height to which a liquid with which the end of a composite strip is brought into contact, according to a T test, rises.

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#### The T test is carried out as follows:

- A strip measuring 2  $\times$  20 cm of the fiber/silicone composite was cut;
- a tank containing a colored ink (for example
  25 fountain pen ink);
  - the cut strip of fibrous material was suspended above the ink bath so as to make the strip flush with the ink;
- the 0 level was defined as the meniscus line 30 of the ink on the strip;
  - the composite strip was left in place until the rising front of ink was in equilibrium;
  - the height (H) in millimeters, corresponding to the difference between the O level and the maximum rise level of the ink along the strip, was measured.

The capillary rise is defined by the distance H. The resistance to capillary rise is inversely proportional to H.

#### Results

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The diagrams shown in Figure 2 represent comparisons between the trace of such capillary rises for three strips of fabric:

- 5 the control strip  $\alpha$  on the left corresponds to a strip cut from a nonimpregnated fibrous material coated with 200 g/m² of silicone elastomer on each face;
- the strip  $\beta a$  in the center corresponds to a strip cut from a composite according to the invention, i.e. produced from a polyester-based fibrous material impregnated according to the invention and then coated with 120 g/m<sup>2</sup> of silicone elastomer on each face; and
  - the strip  $\beta$ b on the right corresponds to a strip cut from a composite according to the invention, i.e. produced from a glass-based fibrous material impregnated according to the invention and then coated with 100 g/m<sup>2</sup> of silicone elastomer on each face.

The strips  $(\beta)$  of the silicone architectural membrane (composite) according to the invention has a zero capillary rise, whereas the control strip  $(\alpha)$  has a capillary rise of more than 100 mm.

It may thus be clearly seen that the impregnation according to the invention guards against the capillary rise, which in its absence would occur over the entire specimen.

A formulation capable of satisfying the compromise of a low viscosity suitable for impregnating textiles and of mechanical properties sufficient for the characteristics of the composite has been demonstrated. It should be noted that the properties achieved allow the product to be classified in the range of elastomers; in particular, the elongation and the hardness are typical of this class.

With such a composition, the level of impregnation of the textile is excellent, thereby limiting the capillary rise by infiltration along the fibers of the fabric, which would be poorly sheathed with the hydrophobic polymer.

# EXAMPLE II: Fluid silicone oil compositions according to the invention

The examples below demonstrate that, with very fluid compositions such as those presented, it is possible to cover a wide hardness range of elastomers while maintaining reasonable mechanical properties.

The compositions presented are, as in the first example, prepared cold by simple mixing. However, they were prepared so as to have two parts, A and B, that were combined together in the ratio  $100\ A\ /10\ B$  just before they were used.

Tables (I) and (II) below give these compositions and the properties that they develop.

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TABLE I

	2-1	2-2	2-3			
Part A						
MM <sup>vi</sup> D <sup>vi</sup> DQ resin, containing 0.6% Vi,	92	90	45			
consisting of 17% M, 0.5% Mvi, 75% D,						
1.5% D <sup>vi</sup> and 6% Q						
PolydiMeMeVi $\alpha, \omega$ -vinylsiloxane,	0	0	45			
containing 2.5% Vi and of 0.4 Pa.s						
viscosity						
Tetra Me, tetra Vi tetrasiloxane.	0	2	0			
PolydiMediMehydrogeno, $\alpha,\omega$ -SiH,	8	13	0			
containing 7.5% SiH and of 0.3 Pa.s						
viscosity						
PolydiMehydrogeno, $\alpha, \omega$ -Me <sub>3</sub> of 0.02	0	0	8			
Pa.s viscosity.						
γ-Methacryloxypropyltrimethoxysilane	1	1	1			
γ-Glycidoxypropyltrimethoxysilane	1	1	1 1			
Ethynylcyclohexanol	250	250	250			
	ppm	ppm	ppm			
Part B						
MM <sup>vi</sup> D <sup>vi</sup> DQ resin, containing 0.6% Vi,	96	96	38			
consisting of 17% M, 0.5% Mvi, 75% D,						
1.5% D <sup>vi</sup> and 6% Q						
PolydiMeMeVi $\alpha,\omega$ -vinylsiloxane,	0	0	58			
containing 2.5% Vi and of 0.4 Pa.s						
viscosity						
Tetrabutyl orthotitanate	4	4	4			
Karstedt's catalyst containing 10%	215	215	215			
platinum	ppm	ppm	ppm			
Hardness (Shore A)	40	45	67			
Tensile strength (MPa)	3.6	4.5	0.8			
Elongation at break (%)	150	100	15			
Viscosity of A (mPa.s)	2760	2040	2950			
Viscosity of B (mPa.s)	4150	4190	2480			
Viscosity of A+B (mPa.s)	3400	2250	2920			

TABLE II

	3-1	3-2	3-4	3-3				
Part	Part A							
Suspension containing 25%	35	35	35	35				
reinforcing silica in an $\alpha, \omega$ -								
vinyl PDMS of 1.5 Pa.s								
viscosity								
$\alpha, \omega$ -Vinyl PDMS of 1.5 Pa.s	55	55	35	37				
viscosity								
$\alpha,\omega$ -Vinyl PDMS of 100 Pa.s	5	5	5	12				
viscosity								
PolydiMeMeVi $\alpha, \omega$ -vinylsiloxane	0	0	18	9				
containing 2.5% Vi and of 0.4								
Pa.s viscosity								
PolydiMediMehydrogeno-α,ω-SiH,	1.1	2.3	5	3.8				
containing 7.5% SiH and of 0.3								
Pa.s viscosity								
α,ω-SiH PDMS containing 5% SiH	4.2	0	0	0				
γ-Methacryloxypropyltri-	1	1	1	1				
methoxysilane								
γ-Glycidoxypropyltrimethoxy-	1	1	1	1				
silane								
Ethynylcyclohexanol	500	500	500	400				
	ppm	ppm	ppm	ppm				
Part	: В	T	Г					
Suspension containing 25% of	40	40	40	40				
reinforcing silica in an $\alpha, \omega$ -								
vinyl PDMS of 1.5 Pa.s		:						
viscosity								
$lpha,\omega ext{-vinyl}$ PDMS of 1.5 Pa.s	56	56	56	56				
viscosity								
Tetrabutyl orthotitanate	4	4	4	4				
Karstedt's catalyst containing	215	215	215	215				
10% platinum	ppm	ppm	ppm	ppm				
Hardness (Shore A)	8	30	49	42				
Tensile strength (MPa)	0.76	1	1.5	2.25				
Elongation at break (%)	250	170	65	135				
Viscosity of A (Mpa.s)	2910	3800	2580	4330				

Viscosity of B (mPa.s)	3400	3400	3400	3280
Viscosity of A+B (mPa.s)	3270	4190	2870	4760